

MPI 2026 WORKSHOP PROBLEM

# **CABLE FLEXING, POLYMER DEFORMATION, AND FATIGUE**

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Drexel University

*Together, improving life*



# Background

W.L. Gore & Associates is making cables for the Semiconductor, Aerospace, and Defense industry.

In many of these applications, the cables are being flexed and repeatedly bend for millions of cycles.

We would like to:

- understand better what the mechanical stresses, strains, and strain rates are on the cables for various geometries.
- translate the 'real world' stress, strains and strain rates into an alternative characterization system.
- predict the lifetime for different cable constructions using Fatigue models for the metal conductor and the polymeric insulators



# Applications

## Typical Applications

- Cleanroom automation
- Advanced packaging equipment
- Front-end wafer inspection
- Wafer metrology equipment
- Semiconductor automated optical inspection (AOI)
- Semiconductor processing equipment
- Linear motion stages
- Pick & place equipment
- Wafer handling
- Flat panel display (FPD) manufacturing equipment
- CMOS image sensor (CIS) packaging equipment
- Lens manufacturing equipment

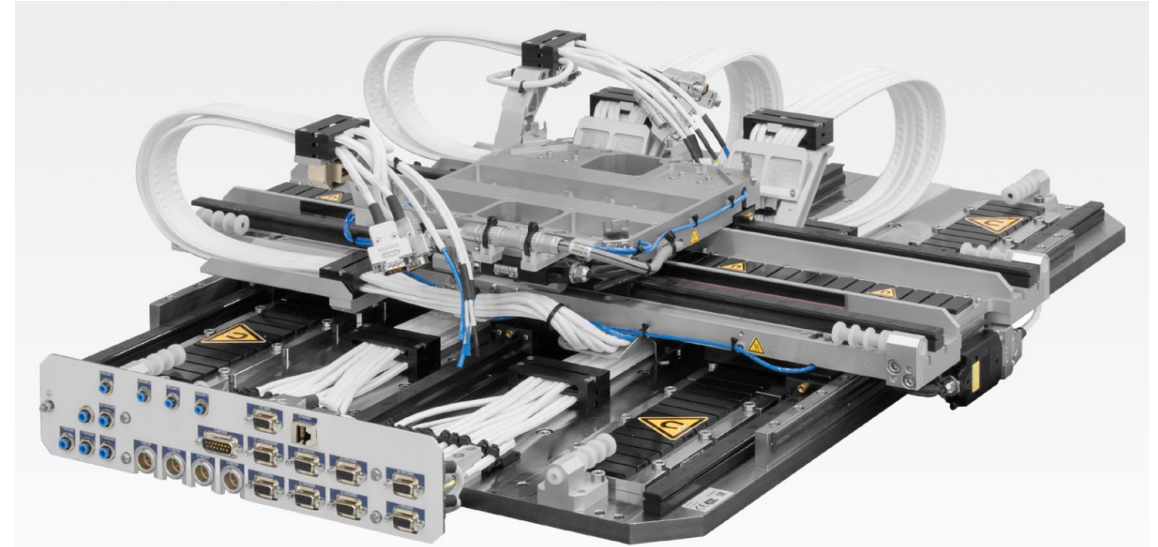
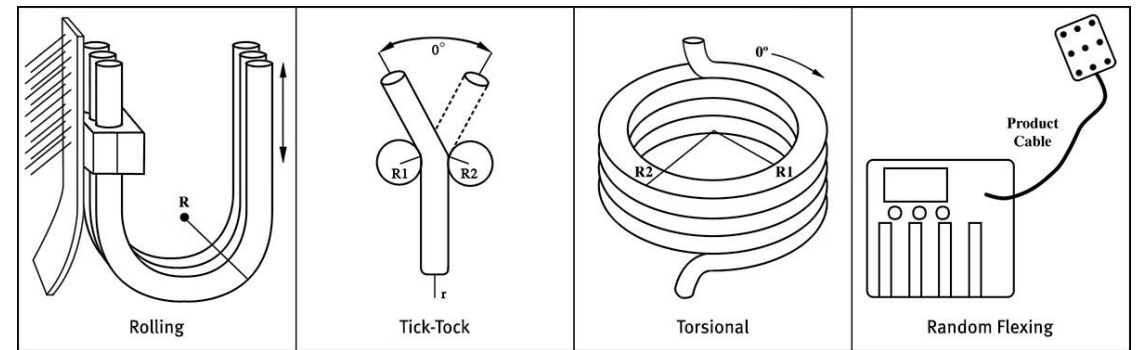


Image courtesy of ETEL S.A.



# Focus for this workshop: Trackless cables

Focus on one cable only, not the entire cable assembly

Used for connecting to movable devices that need power and signal processing

- Often in cleanroom environment, eg, semiconductor industry

## Typical Applications

- Electronic component packaging equipment
- Advanced bonding equipment
- Pick & place mounter equipment
- Back-end manufacturing & inspection processes
- Lens manufacturing equipment
- Manufacturing equipment sensitive to ESD

## Application requirements

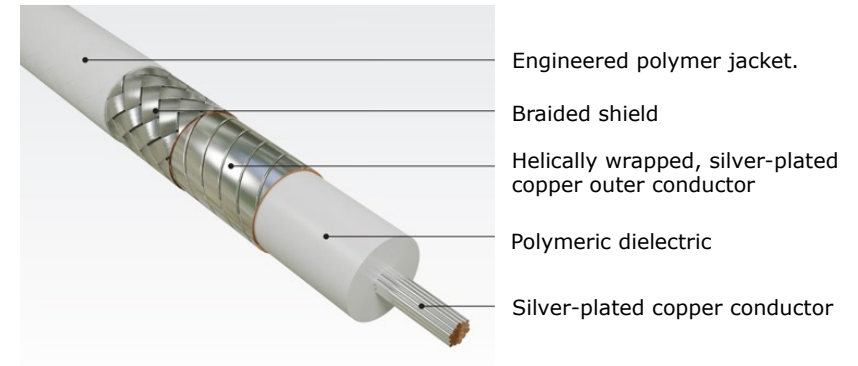
- Maximum Acceleration  $g$  (m/sec<sup>2</sup>) 5.0 (50)
- Speed 5.0 m/sec
- Maximum Self-Supporting Stroke Length 1000 mm
- Overall Width up to 100 mm
- Minimum Bend Radius 50 mm
- Flex Life Cycles > 10 million



# Cable Stress and Failure in High Flex Applications

In its simplest form, a cable is composed of

- (i) a helical stranded Cu conductor
- (ii) a flexible polymer dielectric
- (iii) potentially, a foil or stranded Cu braid shield
- (iv) a polymer jacket



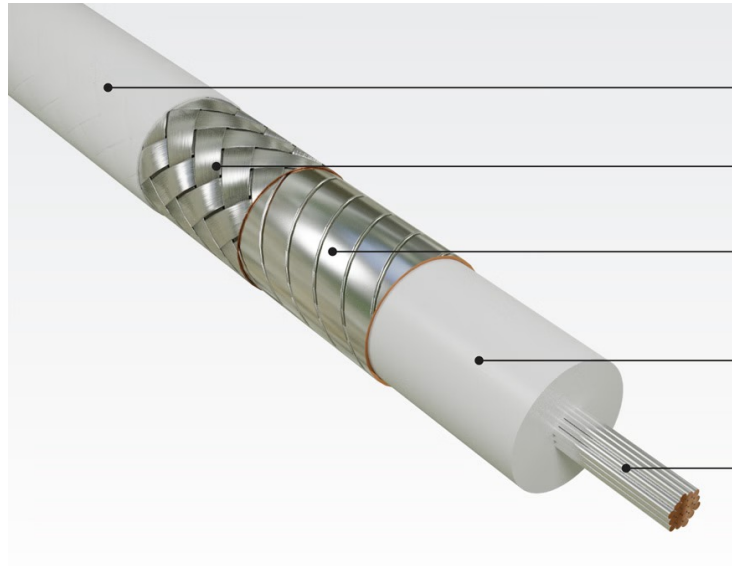
Each time a cable bends or flexes, (i) the helical stranded Cu conductor and potential shield rotates and unfurls to compensate for the strain; (ii) the polymer dielectric and jacket deforms.

- We are primarily interested in the deformation and fatigue of the polymer dielectric

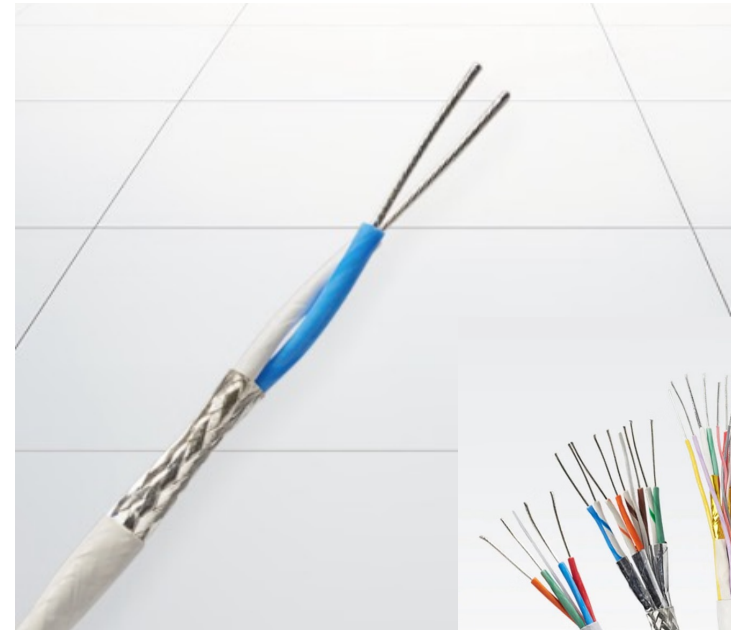
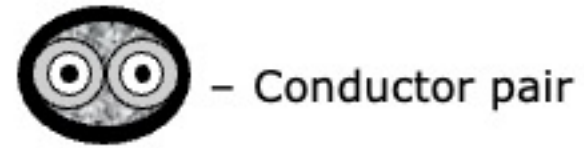
There are three basic causes of failure in any cable subjected to flexing:

- Degradation of the polymer dielectric (=> focus for this MPI workshop!)
- Fatigue of the stranded conductor and shield in the flex area
- Fatigue of the conductor and shield at the point of termination

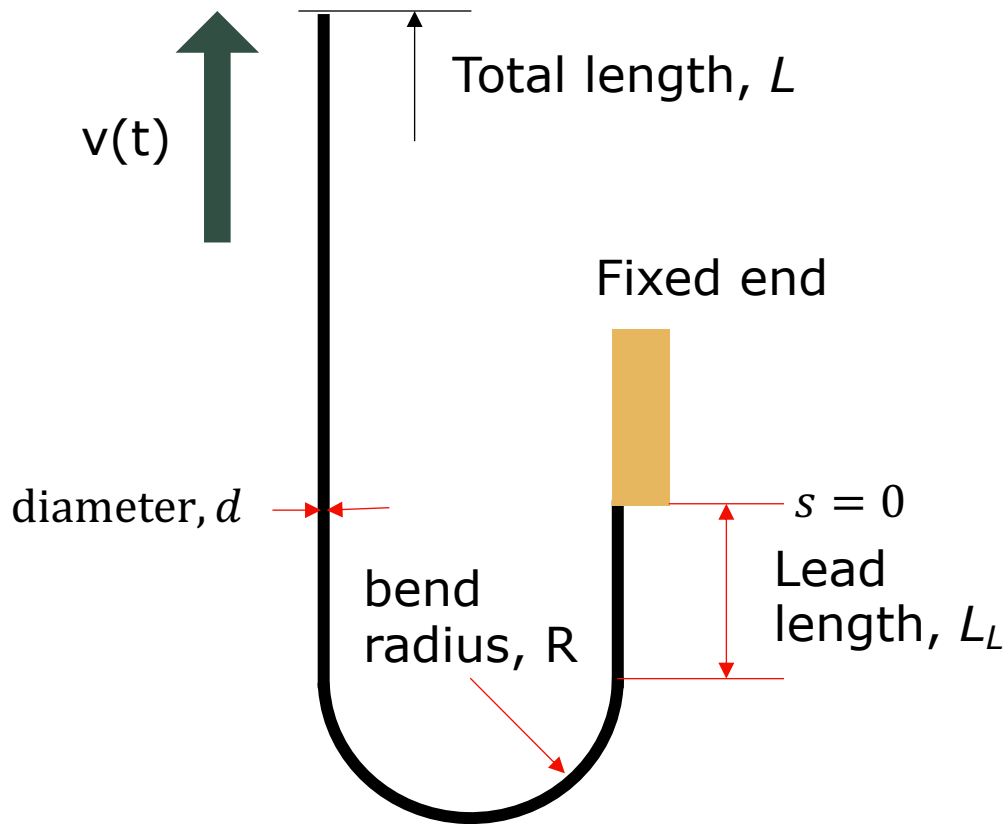
# Cable Geometries



- Engineered polymer jacket.
- Braided shield
- Helically wrapped, silver-plated copper outer conductor
- Polymeric dielectric
- Silver-plated copper conductor



# Cable Cycling – problem definition



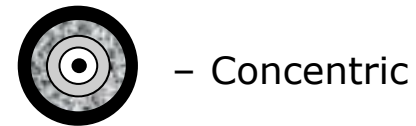
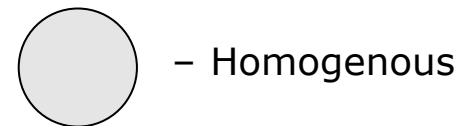
Cable end travels between 0.1m and 1m at various velocity profiles  $v(t)$

Cable cycles at  $\sim 1\text{Hz}$  for  $\sim 10$  million cycles

Geometry varies ( $L, L_L, d, R$ )

Application requirements:  $v(t)$ , (stroke length, acceleration)

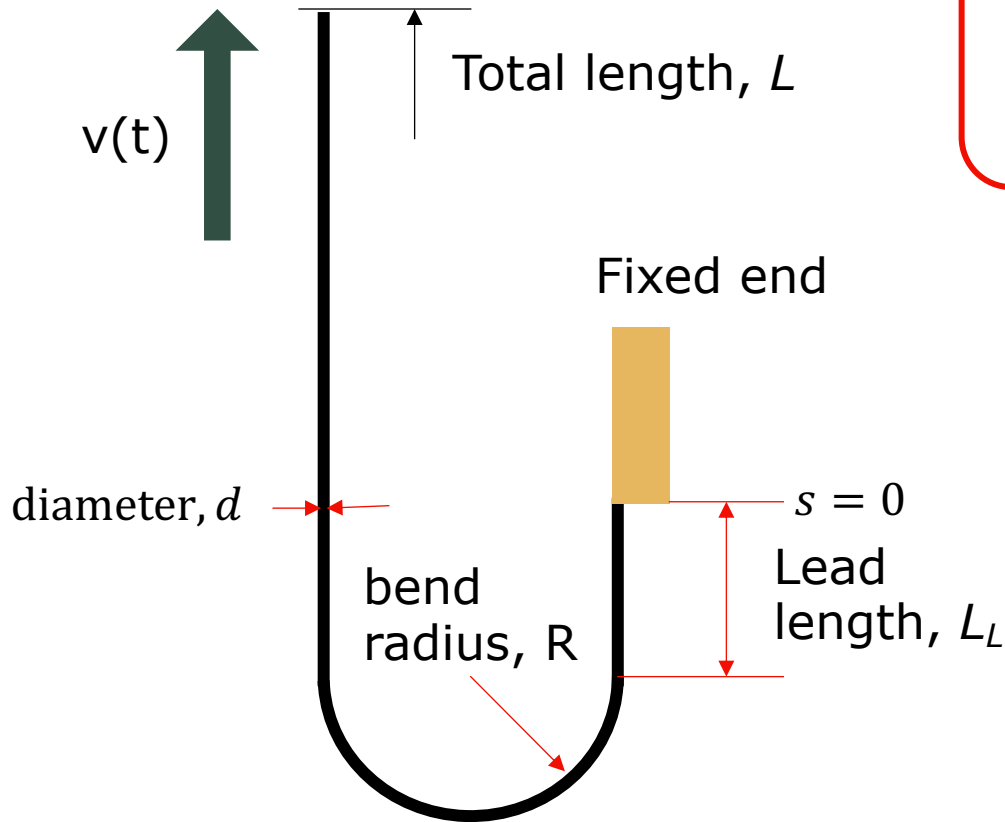
Cross-section of cable varies based on simplification:



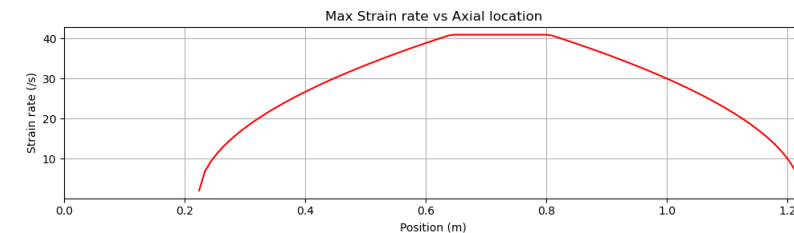
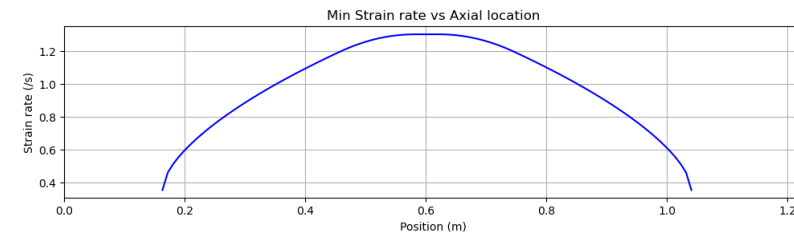
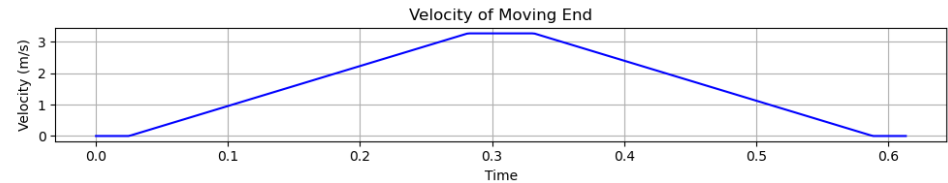
# Cable Cycling – A specific use case

At an acceleration of 1.2g, bend radius (R) of 40mm, stroke length of 0.3m,  $v(t)$  would be 1.64m/sec.

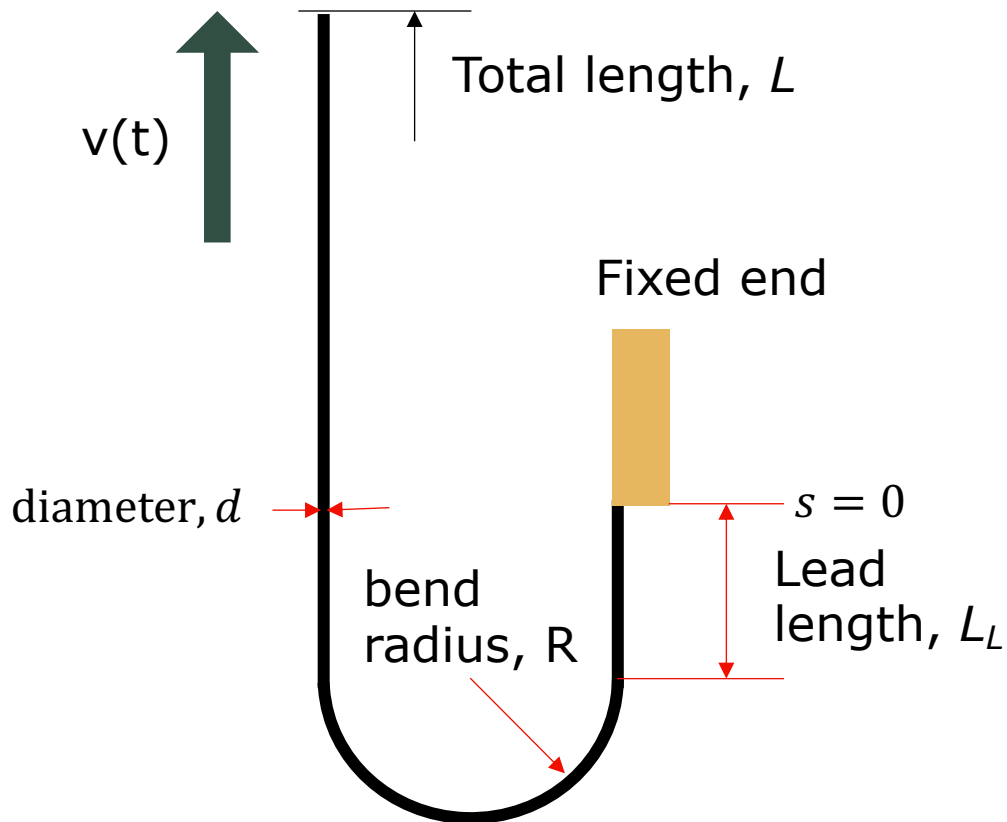
At an acceleration of 2g, bend radius of 40mm, stroke length of 0.3m,  $v(t)$  would be 1.98m/sec.



## Example:

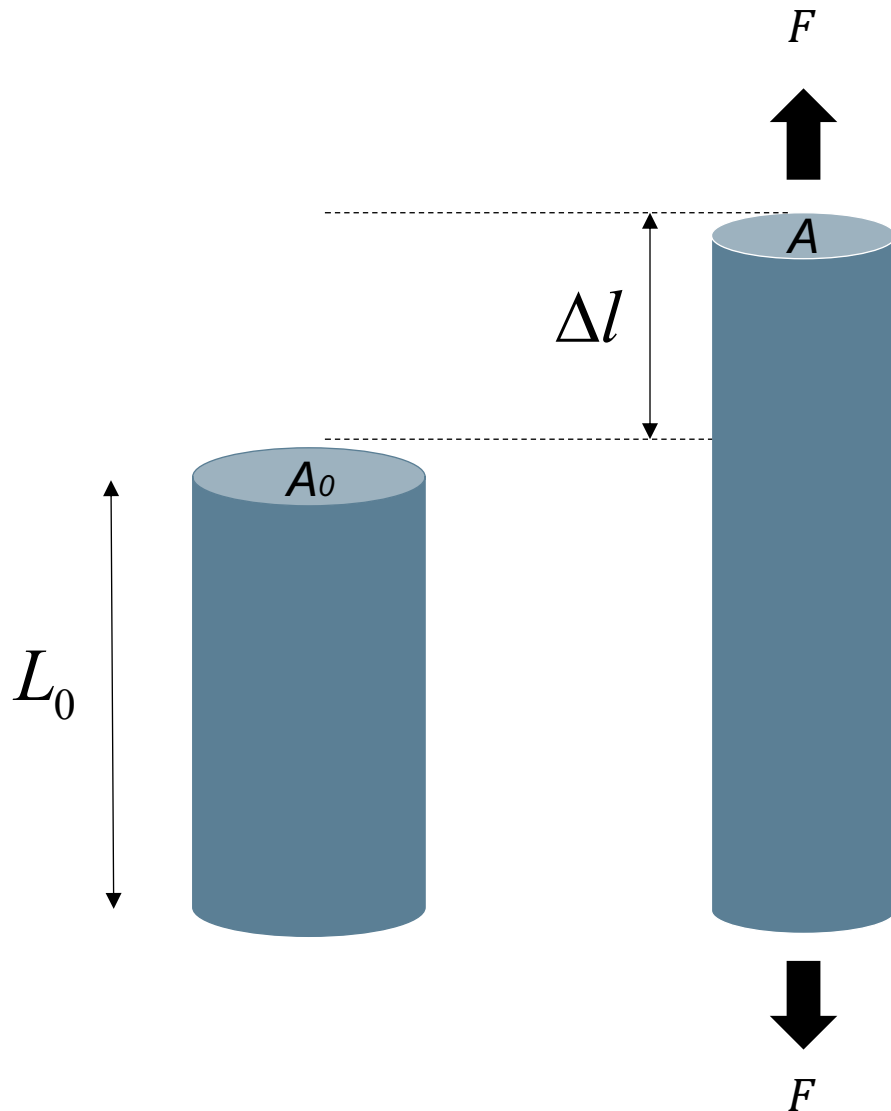


# Cable Cycling - questions



1. What is the stress, strain, and strain rate inside the cable at different cycling velocities and cable geometries?
2. How does the polymeric mechanical model change the stress, strain, and strain rate?
3. Polymer materials properties can be highly resolved by torsional shear testing. Can the stress, strain and strain rates of the cycled cable be transformed into torsional shear test inputs?
4. How will the cycle time/velocity change the performance over time?

# Mechanics background: Concepts of Stress & Strain



**Stress:** force over cross-sectional area [Force per area]

$$\sigma = \frac{F}{A_0}$$

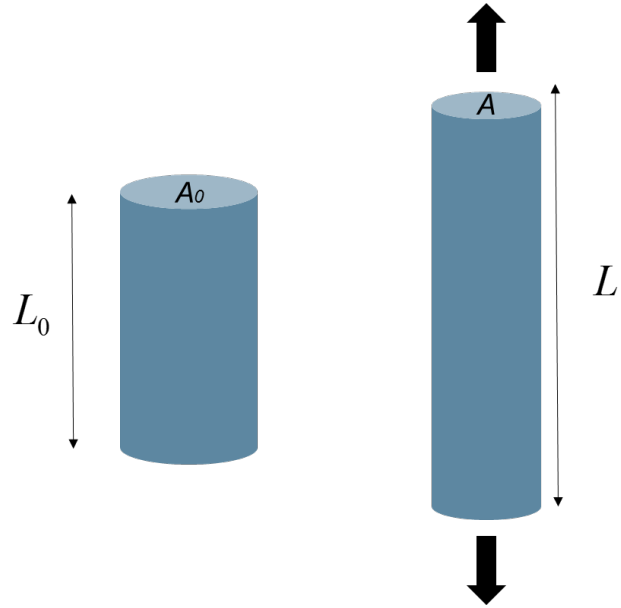
Normalized force  
Units of psi (lbf/in<sup>2</sup>), Pa (N/m<sup>2</sup>)

**Strain:** change in length over initial length [dimensionless]

$$\varepsilon = \frac{\Delta l}{L_0}$$

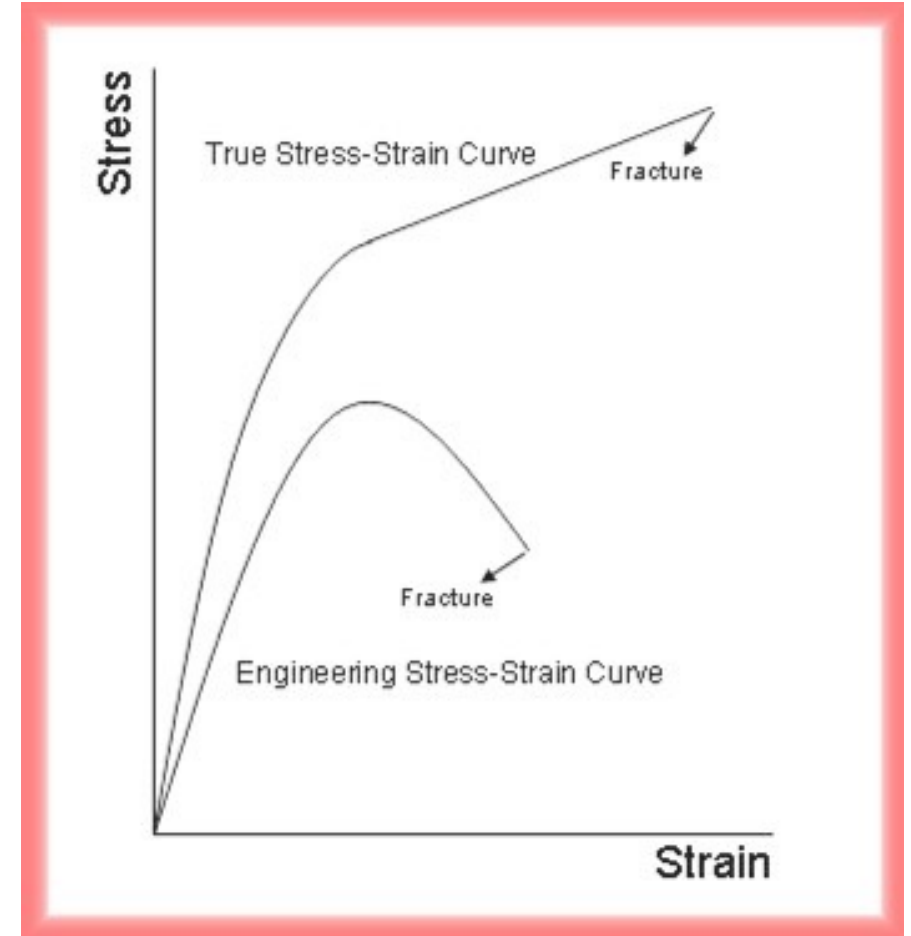
Normalized displacement  
Unitless (or %)  
*0.01 = 1% strain*

# Engineering vs true stress/strain

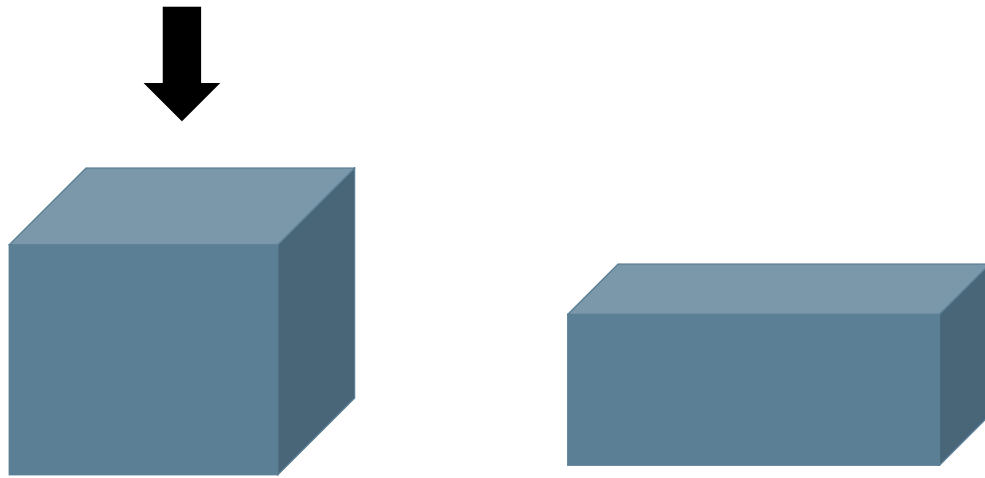


“**Engineering stress/strain**”: normalized by INITIAL length/area

“**True stress/strain**”: normalized by DEFORMED length/area



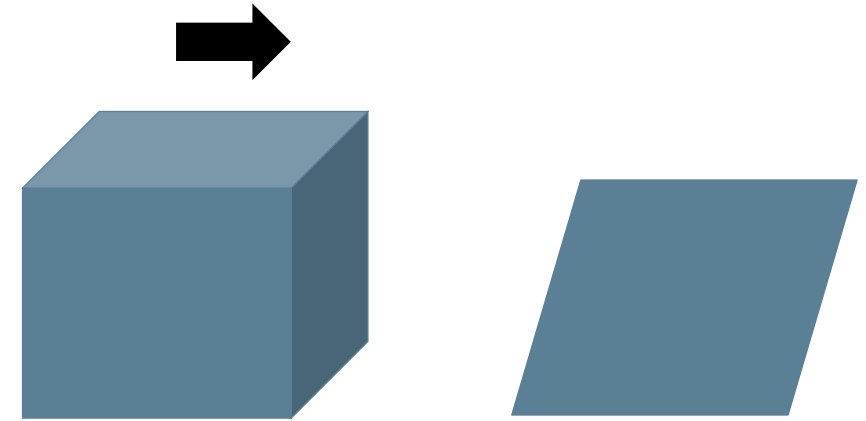
# Normal stress and shear stress



**Normal stress:** force is applied perpendicular to surface

$$\sigma = E \varepsilon$$

*Young's Modulus*



**Shear stress:** force is applied parallel to surface

$$\tau = G \gamma$$

*Shear Modulus*

# Practical applications of 2D Linear Elasticity

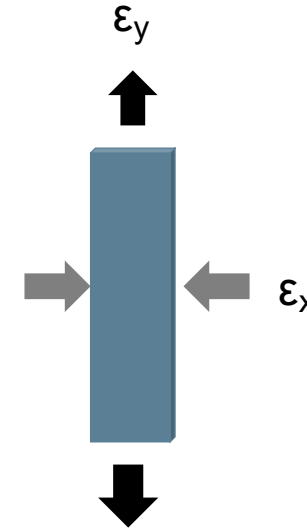
## Poisson's Ratio: 'Necking' of a uniaxial specimen

$$\nu = -\frac{\epsilon_x}{\epsilon_y}$$

No interaction (cork),  $\nu = 0$

Volume preserved (rubber),  $\nu = 0.5$

polymers:  $\nu = \sim 1$  (or larger)



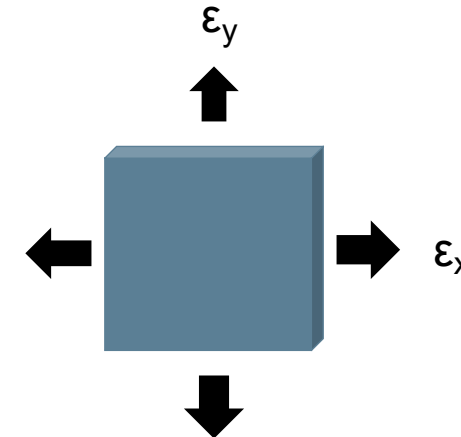
## Biaxial Stretching: Higher stress than same uniaxial stretch (prevent 'necking')

$$Y = \frac{E}{1 - \nu^2}$$

Apparent  
Biaxial Modulus

$$\sigma = Y\epsilon$$

Equi-biaxial stretch  
( $\epsilon_x = \epsilon_y$ )



# Extend to 2D: Plane Stress Hooke's law

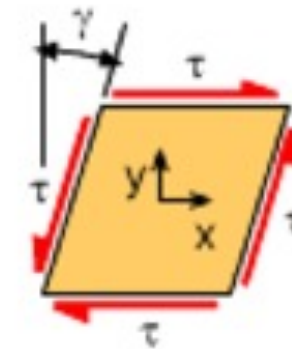
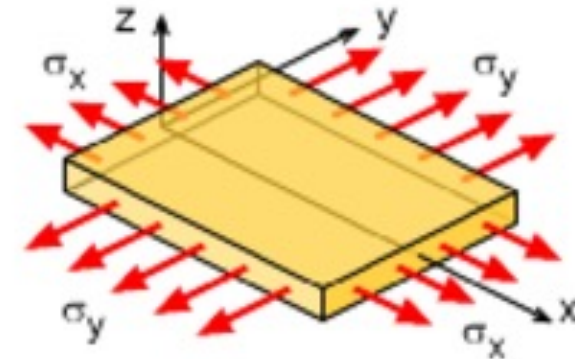
$$\sigma_x = \frac{E}{1 - \nu^2} \epsilon_x + \frac{\nu E}{1 - \nu^2} \epsilon_y$$

$$\sigma_y = \frac{\nu E}{1 - \nu^2} \epsilon_x + \frac{E}{1 - \nu^2} \epsilon_y$$

Normal stress

$$\tau = G\gamma = \frac{E\gamma}{2(1 + \nu)}$$

Shear stress

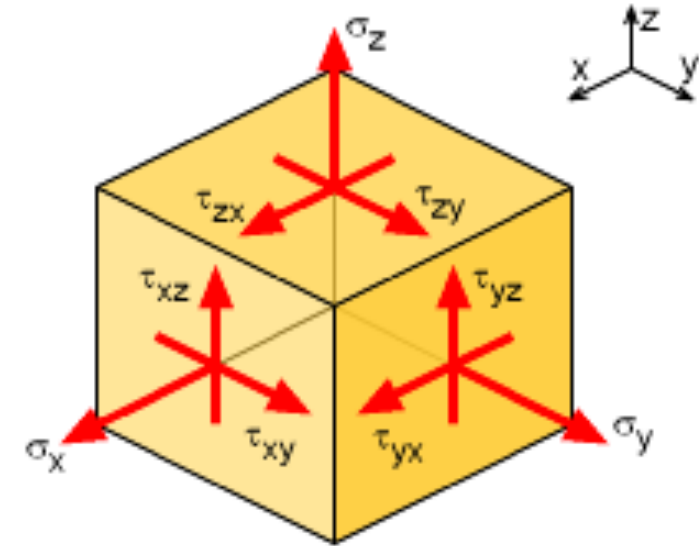


Key parameters: **Young's modulus ( $E$ )**  
**Poisson's Ratio ( $\nu$ )**  
**Shear modulus ( $G$ )** can be calculated from  $E$  and  $\nu$  (not independent)

# Extension to 3D linear elasticity

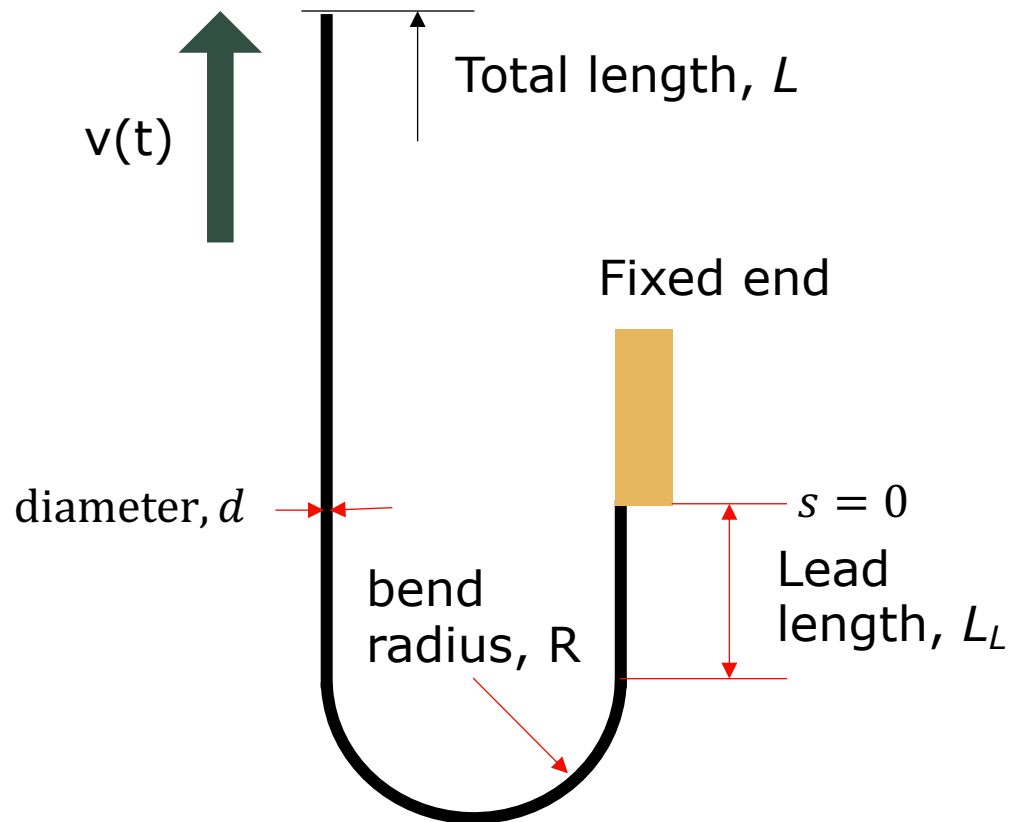
Same material properties ( $E$ ,  $\nu$ ),  
but in 3 directions

Enables analysis of more complex  
loading states



$$\begin{aligned}\sigma_x &= \frac{E}{(1+\nu)(1-2\nu)} \left[ (1-\nu)\epsilon_x + \nu(\epsilon_y + \epsilon_z) \right] \\ \sigma_y &= \frac{E}{(1+\nu)(1-2\nu)} \left[ (1-\nu)\epsilon_y + \nu(\epsilon_z + \epsilon_x) \right] \\ \sigma_z &= \frac{E}{(1+\nu)(1-2\nu)} \left[ (1-\nu)\epsilon_z + \nu(\epsilon_x + \epsilon_y) \right] \\ \tau_{xy} &= G\gamma_{xy}; \quad \tau_{yz} = G\gamma_{yz}; \quad \tau_{xz} = G\gamma_{xz}\end{aligned}$$

# Cable Cycling - questions



1. What is the stress, strain, and strain rate inside the cable at different cycling velocities and geometries?
  - See Slides 17 with 7, 9 (use case acceleration, bend radius, stroke length) and 6 (suggested cable geometries)
2. How does the polymeric mechanical model change the stress, strain, and strain rate?
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# In cylindrical coordinates

Elastic constants  $C_{ij}$  can be different in different directions

- similar to Young's Modulus

For certain boundary conditions, this system can be solved analytically for constant  $C_{ij}$

- Extension, torsion, bending, shearing, pressuring

See Literature list at end of presentation

Limitation: constant  $C_{ij}$  - *linear elastic model*

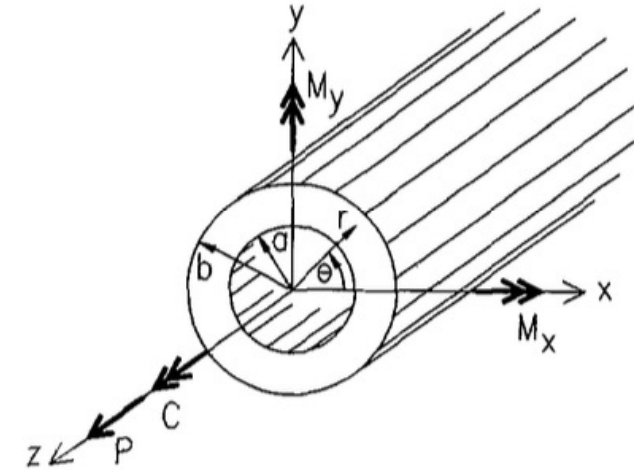
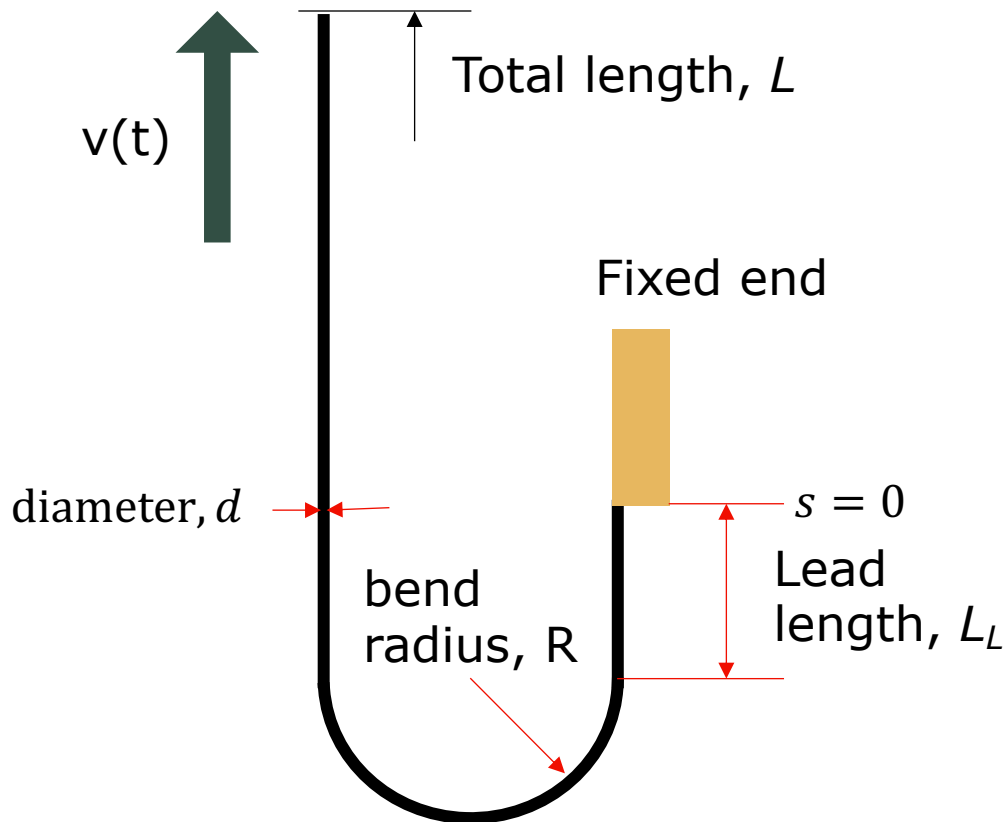


FIG. 1. Cylinder under Study and Applied Loads

$$\begin{Bmatrix} \epsilon_r \\ \epsilon_\theta \\ \epsilon_z \\ \gamma_{\theta z} \\ \gamma_{rz} \\ \gamma_{r\theta} \end{Bmatrix} = \begin{bmatrix} C_{11} & C_{12} & C_{13} & C_{14} & 0 & 0 \\ & C_{22} & C_{23} & C_{24} & 0 & 0 \\ & & C_{33} & C_{34} & 0 & 0 \\ & & & C_{44} & 0 & 0 \\ & \text{sym} & & & C_{55} & C_{56} \\ & & & & & C_{66} \end{bmatrix} \begin{Bmatrix} \sigma_r \\ \sigma_\theta \\ \sigma_z \\ \tau_{\theta z} \\ \tau_{rz} \\ \tau_{r\theta} \end{Bmatrix}$$

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# Polymer Mechanical Models

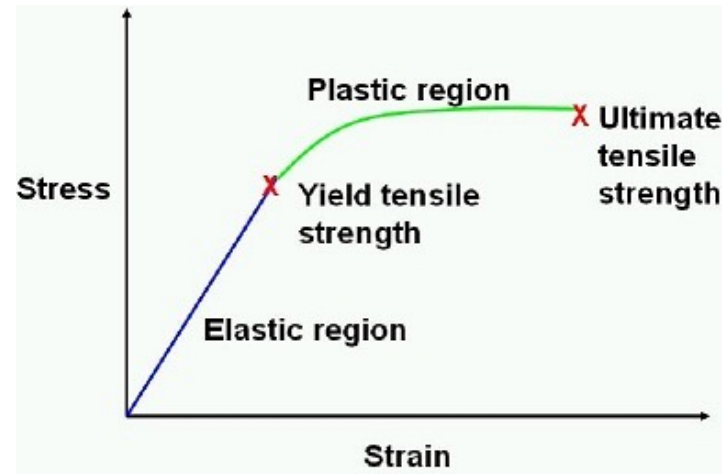
## (1) Linear Elastic



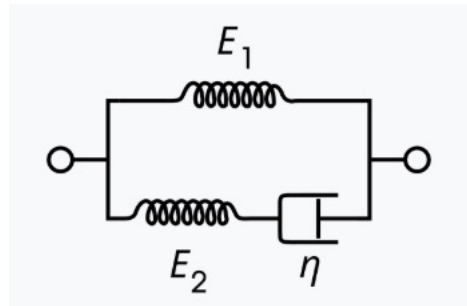
$$\sigma = E \varepsilon$$

*constitutive law* linking stress and strain

E = Young's modulus

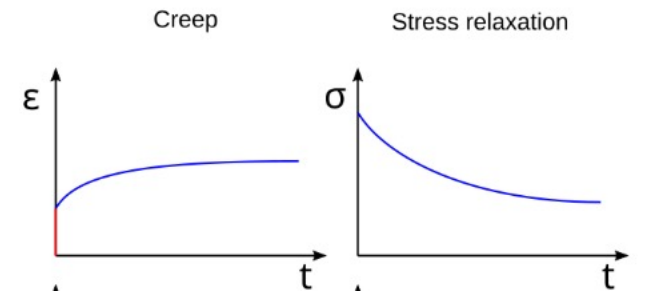


## (2) Viscoelastic (Maxwell 3 component system)



$$\sigma + \frac{\eta}{E_2} \dot{\sigma} = E_1 \varepsilon + \frac{\eta(E_1 + E_2)}{E_2} \dot{\varepsilon}$$

Three-element solid  
(Zener model/SLS)



## Question 2: What if $C_{ij}$ are not constant?

Cylindrical coordinates  $z, r, \theta$

Strain  $\varepsilon_i$ , shear  $\gamma_{ij}$  in all directions

We would like to know how to solve this for non constant  $C_{ij}$  and for rate dependent strain/stresses !!

- E.g., viscoelastic deformation
- Elastic factors  $C_{ij}$  are functions of strain and strain rate
- How to determine Stresses  $\sigma_i$ , shear stresses  $\tau_{ij}$
- Focus on bending first

First step simplification

- Start with 0, 90, 180, 270 degrees
- There, we have tension, compression, torsion only

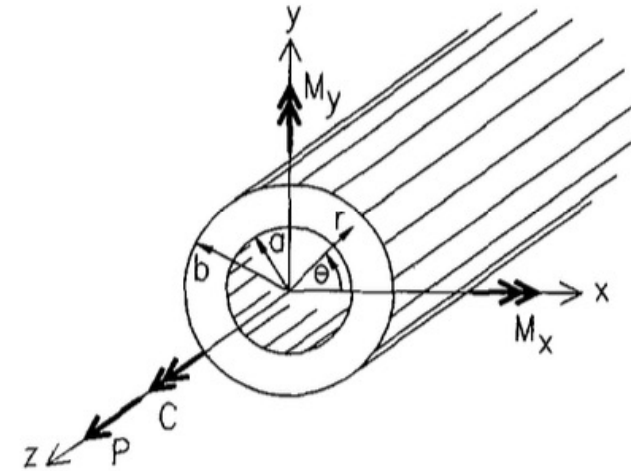
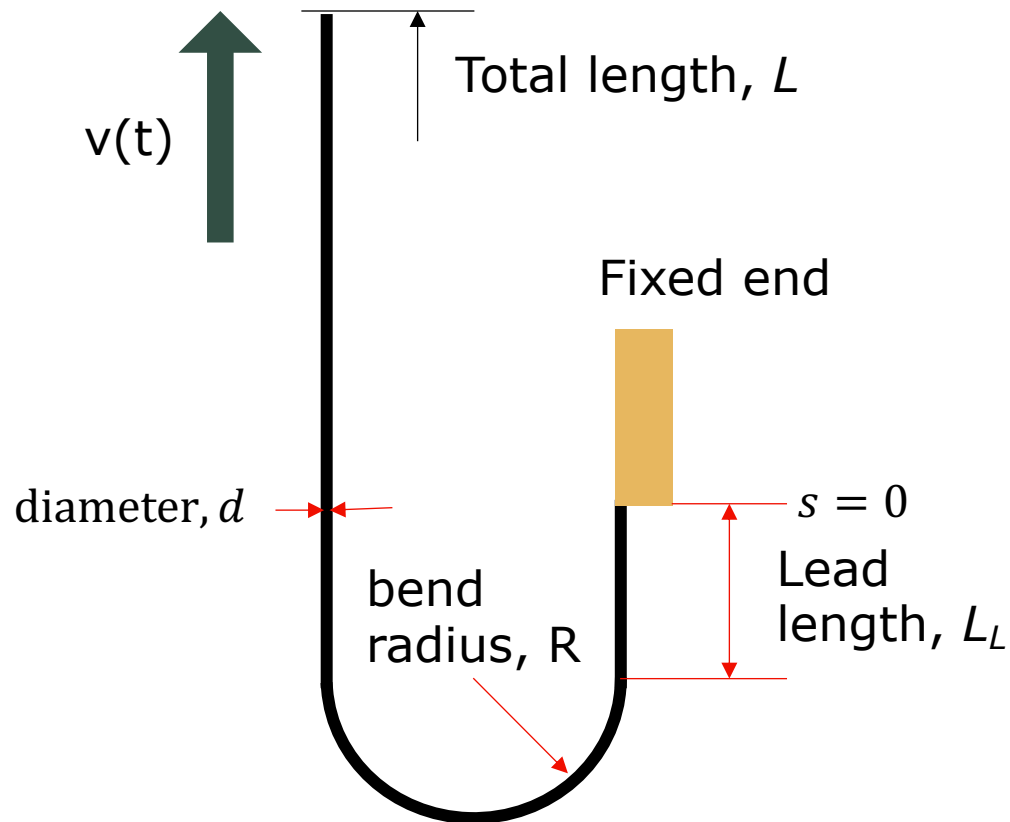


FIG. 1. Cylinder under Study and Applied Loads

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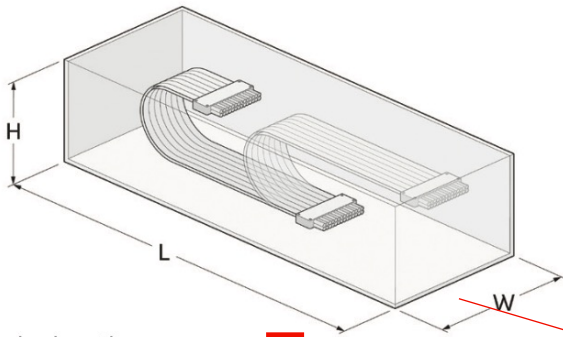
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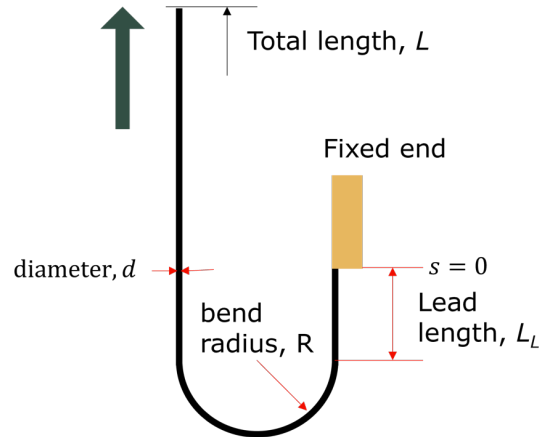
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  - See Slides 23-25
4. How will the cycle time/velocity change the performance over time?

# Question 3: Translating Cable Flexural Behavior to Torsional Shear

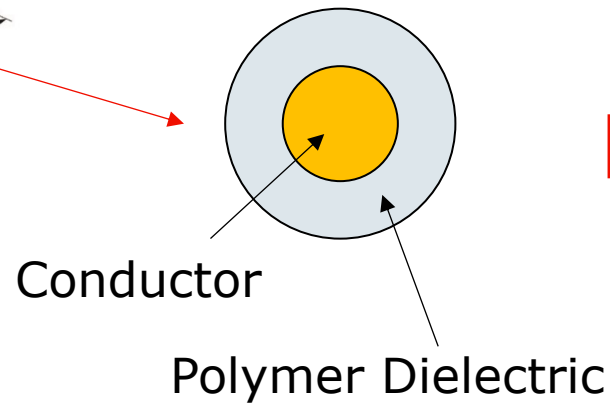
## Application Flexing Stress/Strain State



L = Length  
W = Width  
H = Height

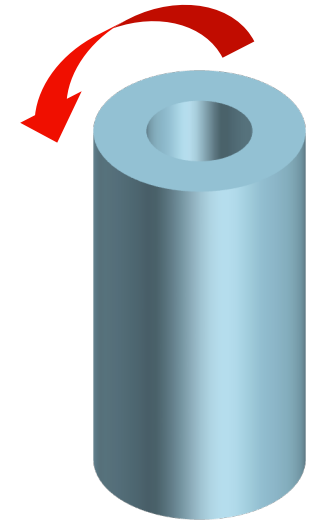
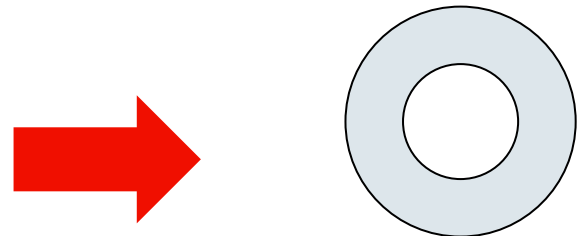


## Simplified Individual Cable Cross section

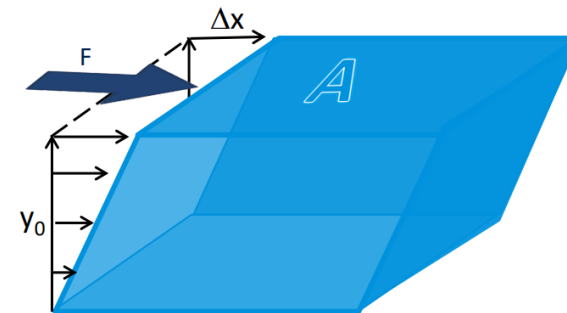


## Characterize the 'formed' polymer dielectric Using Dynamic rheometers in torsion

- Removing the conductor



'formed' Polymer dielectric



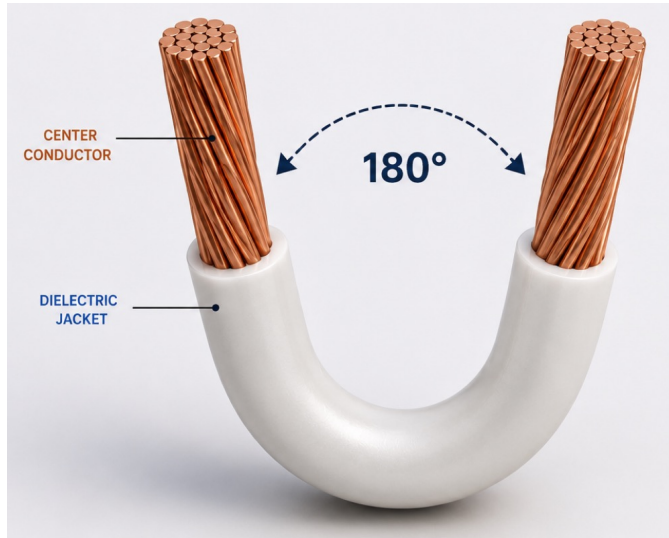
$$\text{Shear stress } \sigma = \frac{F}{A}$$

$$\text{Shear strain } \gamma = \frac{\Delta x}{y_0}$$

$$\text{Shear rate } = \dot{\gamma} = \frac{1}{y_0} \cdot \frac{dx(t)}{dt}$$

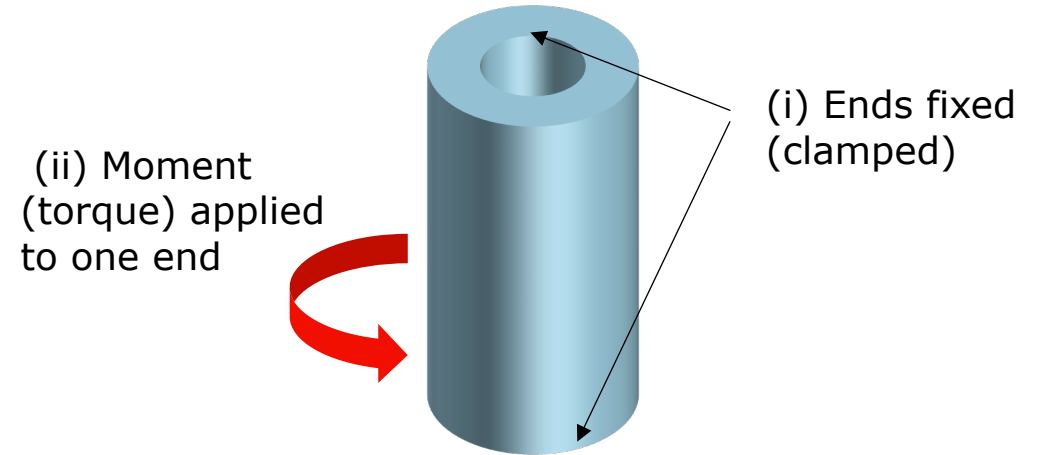
# Translating Cable Flexural Behavior to Torsional Shear

## Application Flexing Stress/Strain State



What are the stress, strain and strain rates in the dielectric during flexing?

## Testing torsional Stress/Strain State



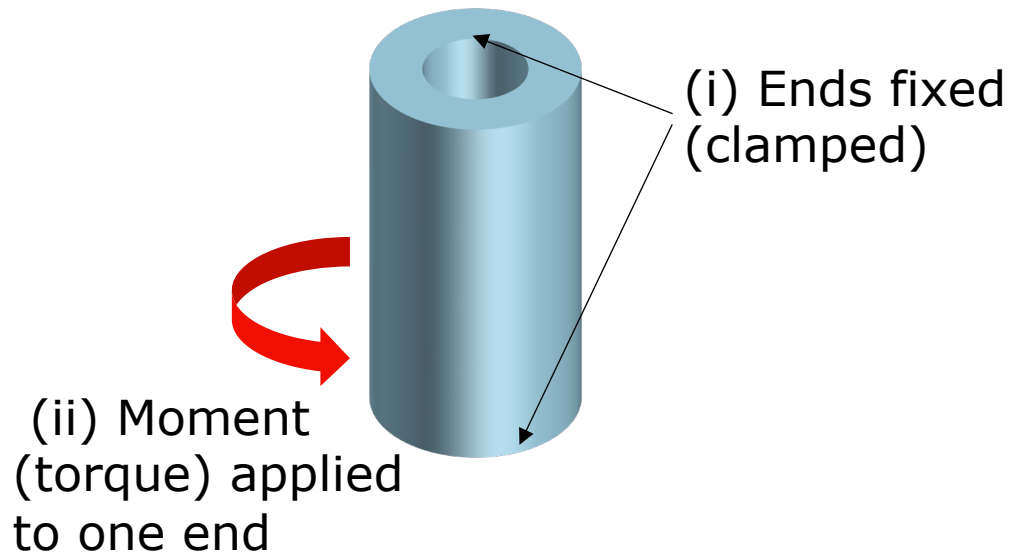
Can the stress, strain and strain rates be translated into:

- (i) shear stress;
- (ii) angular displacement (strain);
- (iii) angular velocity (strain rate)



# Translating Cable Flexural Behavior to Torsional Shear

## Testing torsional Stress/Strain State



## Shear Stress

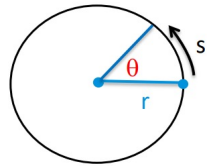
$$\sigma = M \cdot K_{\sigma} \quad M = r \cdot F \cdot \sin \theta$$

$K_{\sigma} = \text{stress constant}$

## Angular Displacement

$$\theta = s/r \quad S = \text{arc length}$$

$r = \text{radius of circle}$



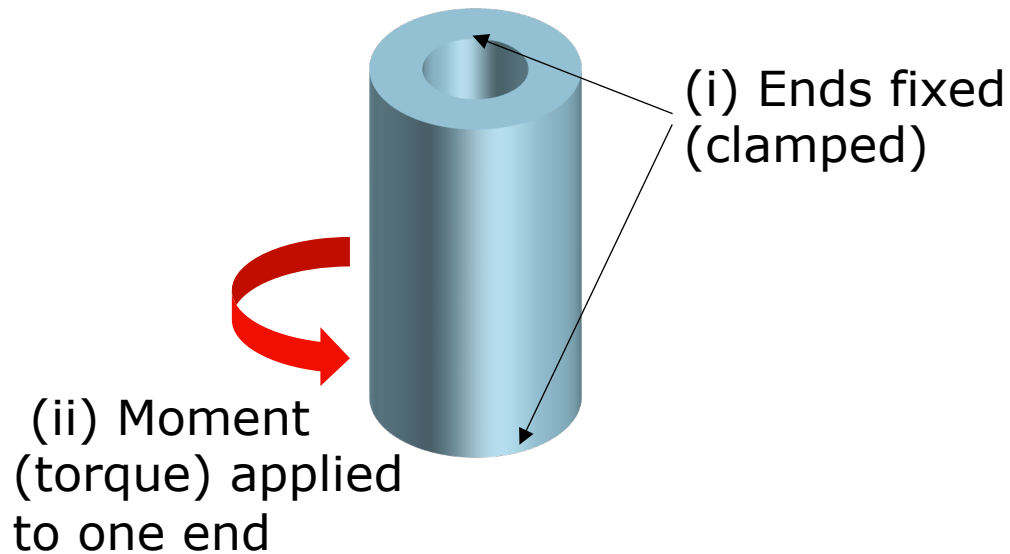
## Shear Strain

$$\gamma = \theta \cdot K_{\gamma}$$

$$\text{Modulus } G = \frac{\sigma}{\gamma} = \frac{M \cdot K_{\sigma}}{\theta \cdot K_{\gamma}}$$

# Translating Cable Flexural Behavior to Torsional Shear

## Testing torsional Stress/Strain State



## Shear Stress

$$\sigma = M \cdot K_{\sigma}$$

$$M = r \cdot F \cdot \sin \theta$$

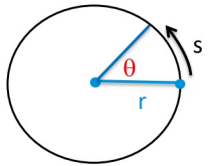
$$K_{\sigma} = \text{stress constant}$$

## Angular Displacement

$$\theta = s/r$$

S = arc length

r = radius of circle



## Shear Strain

$$\gamma = \theta \cdot K_{\gamma}$$

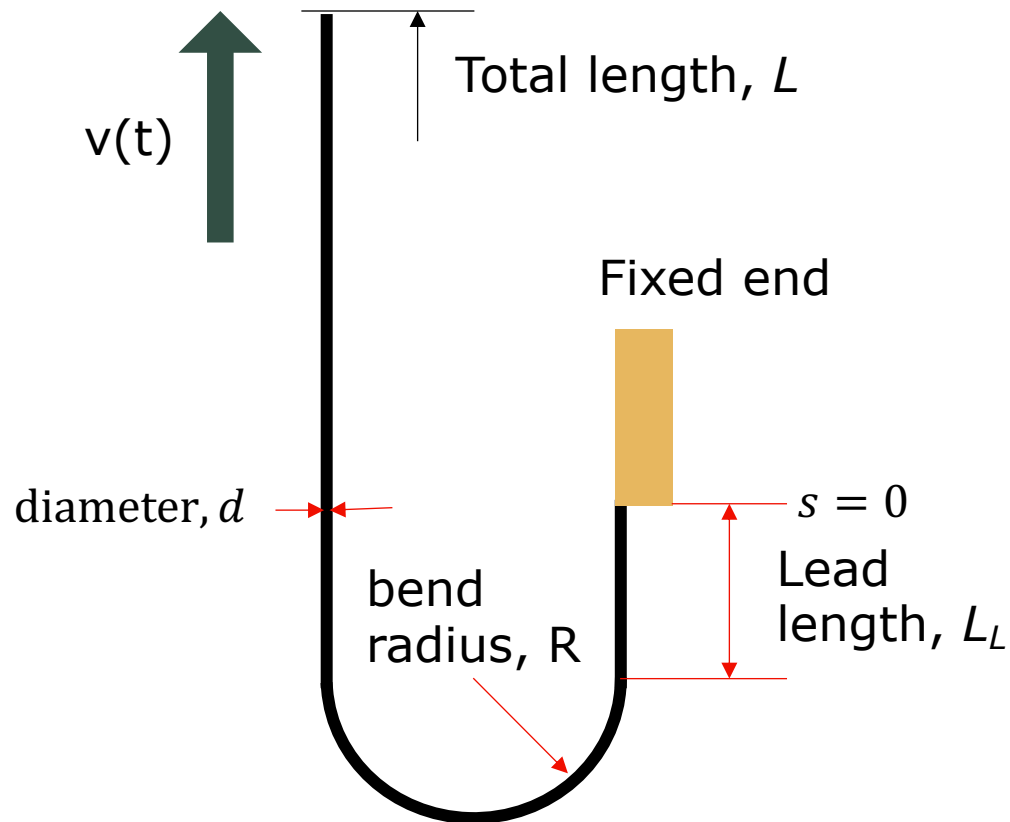
## Angular Velocity

$$\Omega = \frac{\Delta \theta}{\Delta t}$$

## Shear Rate

$$\dot{\gamma} = \Omega \cdot K_{\gamma}$$

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  - See Slides 23-25
4. How will the cycle time/velocity change the performance over time?
  - Polymer degradation and/or fatigue, see Slide 27-28

# Polymer degradation and/or fatigue

Polymers change their behavior over time, which eventually leads to failure

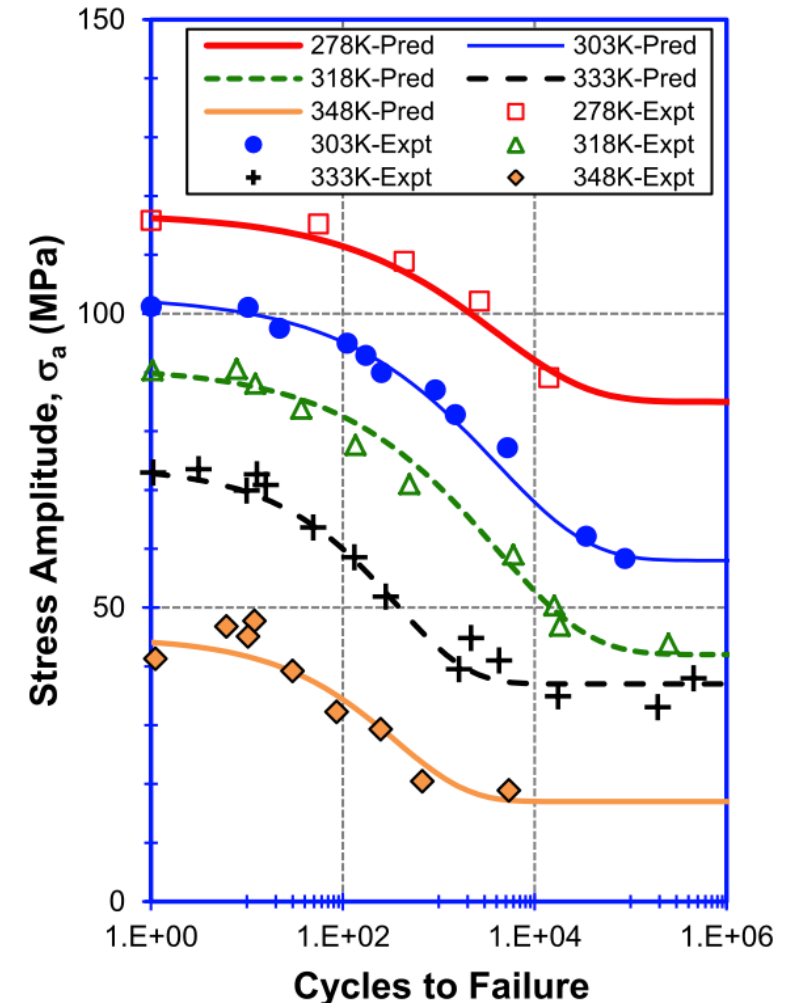
The mechanisms are well understood for metals, but not so much for polymers.

Two groups of failure mechanisms exist:

- Mechanical fatigue by crack propagation
- Thermal fatigue by self heating and thermal softening

Several Models exist to describe the Stress-Life behavior (or S-N curve)

- Mostly are empirical,  $\sigma_a = A (N_f)^B$ 
  - where  $\sigma_a$  is stress amplitude,  $N_f$  is cycles to Failure, A and B empirical constants
- Some are based on physical descriptions of crack propagation



# Polymer degradation and/or fatigue

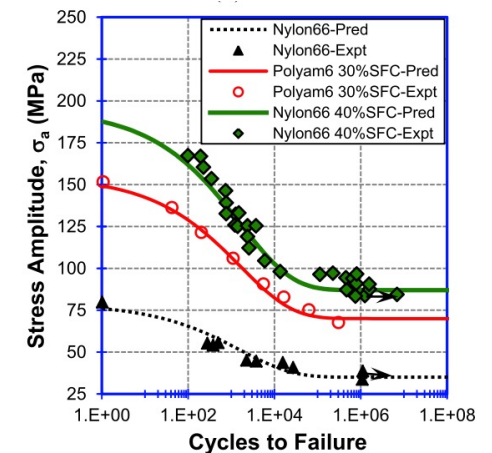
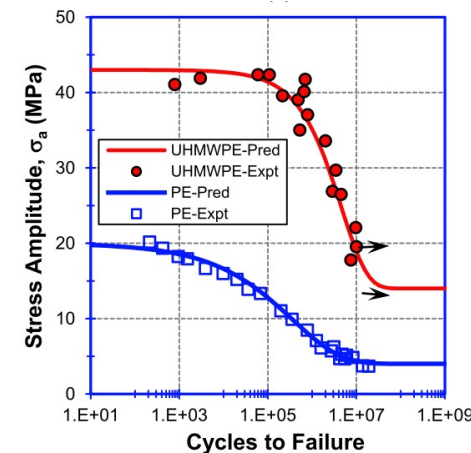
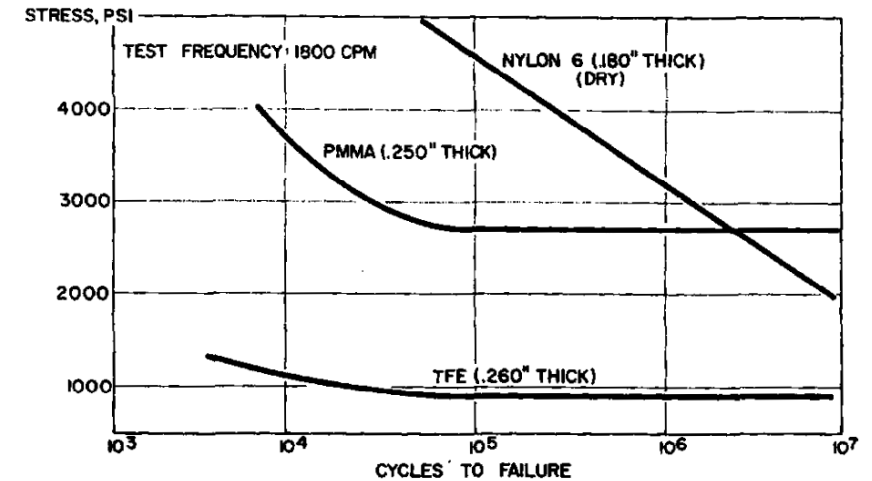
For Gore, it would be interesting to see how different polymers would be influenced by the cycling.

Solid material models do not exist, so we have to rely on crack propagation models and these are influenced by the polymer type.

We may use information from the provided references or search for more.

– Particularly for viscoelastic materials

This question may be beyond the scope for the one-week MPI.



# References

## Stress Analysis

C. Jolicoeur and A. Cardou, "Analytical Solution for Bending of Coaxial Orthotropic Cylinders, J Eng Mech 120 (1994), 2556

L.P. Kollar and G.S. Springer, "Stress Analysis of Anisotropic Laminated Cylinders and Cylindrical segments", In J Solids Struc 29 (1992), 1499

J.Q. Tarn and Y.M. Wang, "Laminated Composite Tubes under extension, torsion, bending, shearing and pressuring: a State Space Approach", In J Solids Stuc 38 (2001), 9053

C. McCorquodale, "Development of a Fatigue Analysis Tool to Predict Cable Flex Life", PhD Dissertation, Edinburgh Napier University, 2014

## Fatigue

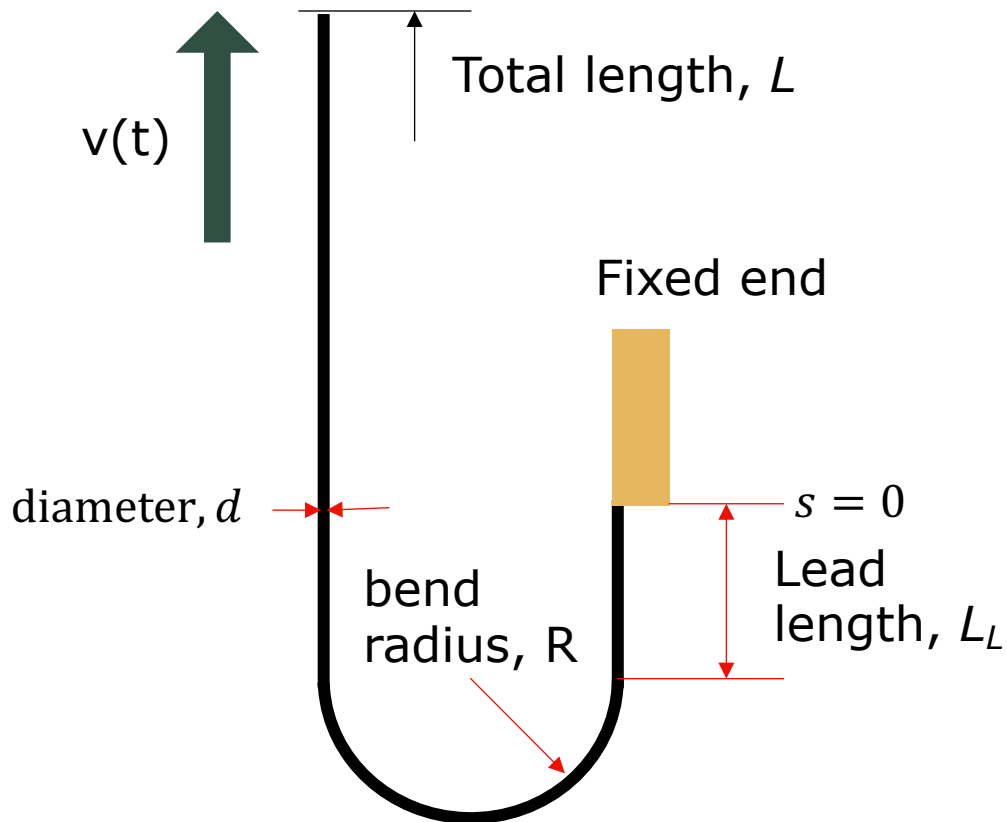
H.S. Kim, "Prediction of S-N curves at various stress ratios for structural Materials", Proc Struc Integr 19 (1019), 472

K.S.R. Chandran, "Mechanical Fatigue of Polymers: A new Approach to characterize the S-N behavior on the Basis of Macroscopic Crack Growth Mechanism", Polymer 91 (2016), 222

S. Maiti and P.H. Geubelle, "A Cohesive Model for Fatigue Failure of Polymers", Eng Frac Mech 72 (2005), 691

M.N. Ridell, G.P. Koo, and J.L. O'Toole. "Fatigue Mechanisms of Thermoplastics", Polym Eng Sci 6 (1966), 363

# Cable Cycling – any questions



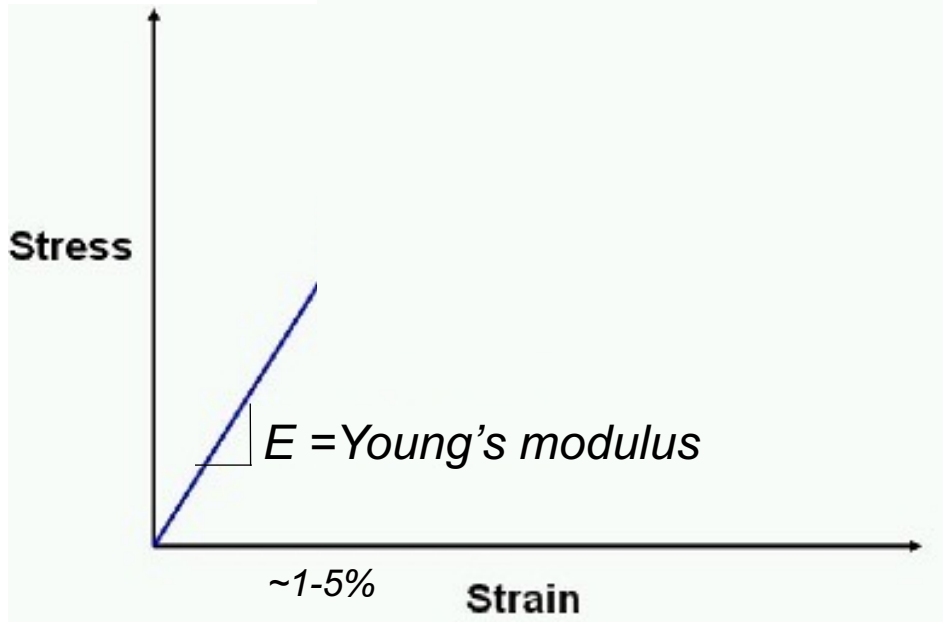
1. What is the stress, strain, and strain rate inside the cable at different cycling velocities and geometries?
  - See Slides 17 with 7, 9 (use case acceleration, bend radius, stroke length) and 6 (suggested cable geometries)
2. How does the polymeric mechanical model change the stress, strain, and strain rate?
  - See Slides 19 and 20 (elastic vs visco elastic)
3. Polymer materials properties can be highly resolved by torsional shear testing. Can the stress, strain and strain rates of the cycled cable be transformed into torsional shear test inputs?
  - See Slides 23-25
4. How will the cycle time/velocity change the performance over time?
  - Polymer degradation and/or fatigue, see Slide 27-28

# APPENDIX

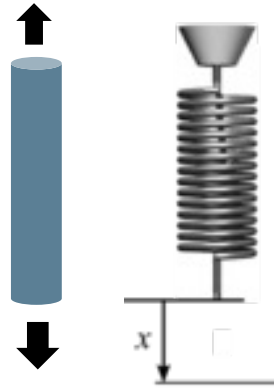
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# Starting simple: 1D Linear Elasticity (Hooke's Law)



<http://physics.tutorvista.com/fluid-dynamics/strain.html>



## Hooke's Law:

$$\sigma = E \varepsilon$$

*constitutive law* linking stress and strain

$E$  = Young's modulus

### Example values:

Stainless Steel	$E = 200 \text{ Gpa}$
Copper	$E =$
ePTFE	$E = 10 \text{ MPa} - 1 \text{ GPa}$
PATT	$E = 1 - 10 \text{ MPa}$
FEP	$E = 650 \text{ MPa}$
Jello	$E = 1 - 100 \text{ kPa}$